Chapter #2

EEE8013 - EEE3001

State Space Analysis and Controller Design

Contents

1. Introduction and Motivation Example

Assume that we have an n^{th} order system: $x^{(n)} = f\left(x, x', x'', \ldots x^{(n-1)}\right)$. Very difficult to study it as even if it is a linear system we must solve an n^{th} order polynomial equation. Theoretically we can use geometric and/or analytical methods but this can be applied only in some specific cases. Computers can be used to tackle this problem and as they are better with 1^{st} order ODEs we break the n^{th} order ODE to a system of n 1^{st} order ODEs. Also by using matrices we can use powerful tools from linear algebra. The goal of this chapter is to introduce a new approach in the modelling of dynamical systems, the method is called state space analysis and it is far more versatile than the well-known Transfer Functions.

More specifically, the classical control system design techniques (such as root locus and frequency response methods) are generally applicable to:

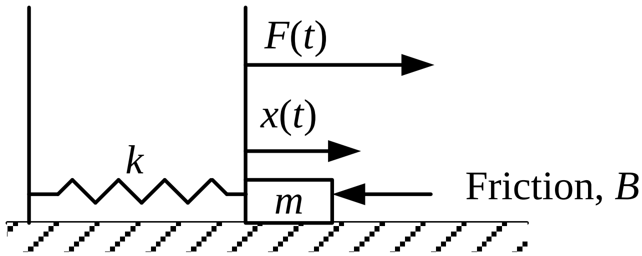
a) Single Input Single Output (SISO) systems
b) Systems that are linear and time invariant (have parameters that do not change with time)

The state space approach is a generalized time domain method for modelling, analysing and designing control systems and is particularly well suited to digital implementation. The state space approach can deal with:

a) Multi Input Multi Output systems
b) Non-linear and time variant systems
c) Alternative controller design approaches

Example:

Assume the simple mass-spring system:



Using Newtonian mechanics we get:

$$\frac{d^2x}{dt^2} = F - B\frac{dx}{dt} - kx = m\ddot{x} = F - B\dot{x} - kx$$

By choosing as $x_1 = x,\ x_2 = \dot{x}$ we have:

$$\left.\begin{aligned} \dot{x}_1 &= \dot{x} = x_2 \\ \dot{x}_2 &= \ddot{x} = \frac{1}{m}\left(F - Bx_2 - kx_1\right) \end{aligned}\right\} \Rightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{B}{m} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ F/m \end{bmatrix}$$

Or $\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{B}{m} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} F \Leftrightarrow \dot{x} = Ax + Bu$

The variables x_1 and x_2 define the state vector x, which in turn defines the state (a complete summary/description) of the system. Knowing the current state and the future inputs we can predict the future states, i.e. the future behaviour of the system. In the aforementioned case, knowing the values/direction of the force F, the current displacement x and speed $\dot{x}$ of the object we can fully define its future displacement and speed.

Example 2.1: Write in a state space form the following system:

$$\left.\begin{aligned}\frac{dx_1}{dt} &= 3x_1 + 2x_2 + u_1 - 3u_2 + 3u_3 \\ \frac{d}{dt} &= -x_1 + 5x_2 + 0.1u_2\end{aligned}\right\} \Rightarrow \frac{d}{dt}\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 3 & 2 \\ -1 & 5 \end{bmatrix}\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & -3 & 3 \\ 0 & 0.1 & 1 \end{bmatrix}\begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$

2. General State Space Model

In a more general case when we have *n* states and *m* inputs we have:

$$\frac{dx_1}{dt} = a_{1,1}x_1 + a_{1,2}x_2 + a_{1,3}x_3 + \dots\dots\dots\dots + a_{1,n}x_n + b_{1,1}u_1 + b_{1,2}u_2 + \dots\dots\dots + b_{1,m}u_m$$

$$\frac{dx_2}{dt} = a_{2,1}x_1 + a_{2,2}x_2 + a_{2,3}x_3 + \dots\dots\dots\dots + a_{2,n}x_n + b_{2,1}u_1 + b_{2,2}u_2 + \dots\dots\dots + b_{2,m}u_m$$

$$\vdots$$

$$\frac{dx_n}{dt} = a_{n,1}x_1 + a_{n,2}x_2 + a_{n,3}x_3 + \dots\dots\dots\dots + a_{n,n}x_n + b_{n,1}u_1 + b_{n,2}u_2 + \dots\dots\dots + b_{n,m}u_m$$

This can be written in a vector form as:

$$\dot{x} = Ax + Bu$$

where:

$$\dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \vdots \\ \dot{x}_n \end{bmatrix}, A = \begin{bmatrix} a_{1,1} & a_{12} & \dots\dots & a_{1,n} \\ a_{2,1} & \dots\dots & \dots\dots & a_{2,n} \\ \dots\dots & \dots\dots & \dots\dots & \dots\dots \\ a_{n,1} & \dots\dots & \dots\dots & a_{n,n} \end{bmatrix}, x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}, B = \begin{bmatrix} b_{1,1} & \dots & \dots & b_{1,m} \\ \dots & \dots & \dots & \dots \\ b_{n,1} & \dots & \dots & b_{n,m} \end{bmatrix}, u = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_m \end{bmatrix}$$

Now, in order to "monitor" the system we need sensors to measure various variables like the displacement and velocity of the mass.

Let's assume that we can buy sensors for both variables (the speed and the displacement), then we define the output of the system to be:

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \Leftrightarrow y = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} x \Leftrightarrow y = Cx$$

Let's assume that we can buy only one sensor, that measures the displacement, then the output is: $y = x_1 \Leftrightarrow y = \begin{bmatrix} 1 & 0 \end{bmatrix} x \Leftrightarrow y = Cx$

Let's assume that we can buy only one sensor, that measures the velocity, then the output is: $y = x_2 \Leftrightarrow y = \begin{bmatrix} 0 & 1 \end{bmatrix} x \Leftrightarrow y = Cx$

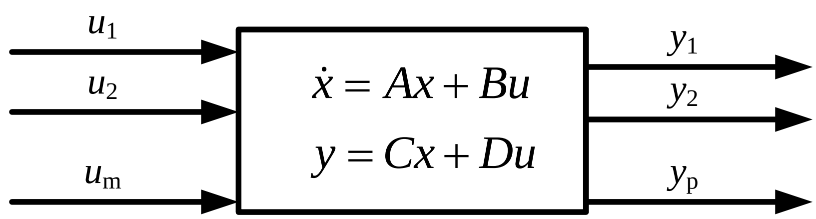
Let's assume that we have only one sensor that measures a linear combination of the displacement and velocity: $y = a_1 x_1 + a_2 x_2 \Leftrightarrow y = \begin{bmatrix} a_1 & a_2 \end{bmatrix} x \Leftrightarrow y = Cx$

Hence, the most general case:

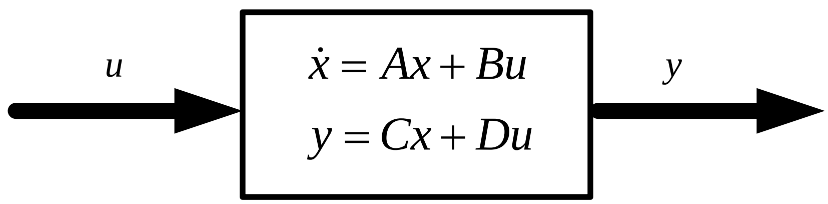
$$\begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_p \end{bmatrix} = \begin{bmatrix} c_{1,1}x_1 + c_{1,2}x_2 + \cdots c_{1,n}x_n \\ c_{2,1}x_1 + c_{2,2}x_2 + \cdots c_{2,n}x_n \\ \cdots \\ c_{p,1}x_1 + c_{p,2}x_2 + \cdots c_{2pn}x_n \end{bmatrix} \Leftrightarrow y = \begin{bmatrix} c_{1,1} & c_{1,2} & \cdots & c_{1,n} \\ c_{2,1} & c_{2,2} & \cdots & c_{2,n} \\ \vdots & \ddots & \cdots & \vdots \\ c_{p,1} & c_{p,2} & \cdots & c_{p,n} \end{bmatrix} x \Leftrightarrow y = Cx$$

Finally let's assume that (in a rather artificial case) that the input can directly influence the output, then we have: $y = Cx + Du$, For some matrix D.

So the system is described by $\begin{matrix} \dot{x} = Ax + Bu \\ y = Cx + Du \end{matrix}$:



Or in a vector form:



Where: $u = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_m \end{bmatrix}, \quad y = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_p \end{bmatrix}$

In general:

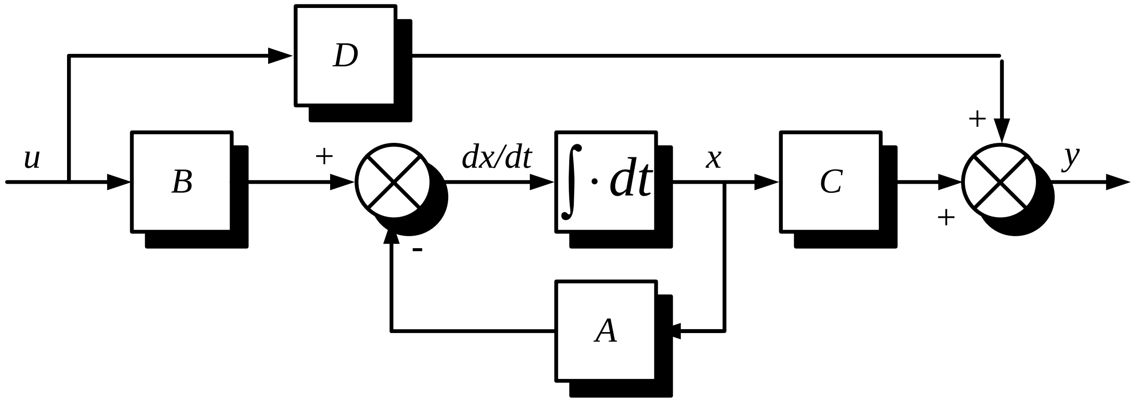
$$\dot{x}(t) = A(t)x(t) + B(t)u(t)$$
$$y(t) = C(t)x(t) + D(t)u(t)$$

Where

- x is an n x 1 state vector, i.e. $x \in \mathbb{R}^{n\times 1}$
- u is an m x 1 input vector, i.e. $u \in \mathbb{R}^{m\times 1}$
- y is an p x 1 output vector, i.e. $y \in \mathbb{R}^{p\times 1}$
- A is an n x n state matrix, i.e. $A \in \mathbb{R}^{n\times n}$
- B is an n x m input matrix, i.e. $B \in \mathbb{R}^{n\times m}$
- C is an p x n output matrix, i.e. $C \in \mathbb{R}^{p\times n}$
- D is an p x m feed forward matrix (usually zero), i.e. $D \in \mathbb{R}^{p\times n}$

If the system is Linear Time Invariant (LTI):

$$\dot{x}(t) = Ax(t) + Bu(t)$$
$$y(t) = Cx(t) + Du(t)$$



The state of a system is a complete summary of the system at a particular point in time. If the current state of the system and the future input signals are known then it is possible to define the future states and outputs of the system.

The state of a system may be defined as the set of variables (state variables) which at some initial time t_o, together with the input variables, completely determine the behaviour of the system for time $t \geq t_o$.

The state variables are the smallest number of variables that can describe the dynamic nature of a system and it is not a necessary constraint that they are measurable. The manner in which a state variables change with time can be thought of as trajectory in n dimensional space called *state space*. Two dimensional state space is sometimes referred to as the phase plane when one state is the derivative of the other.

The choice of the state space variables is free as long as some rules are followed:

- They must be linearly independent.
- They must specify completely the dynamic behaviour of the system.
- Finally they must not be input of the system.

Example 2.2: Find the state space model of the following system:

$$\ddot{x}(t)+3\dot{x}(t)+2x(t)=u(t)$$

$$y=4x(t)$$

$$\left.\begin{array}{l}\dot{x}_1=\dot{x}=x_2\\ \dot{x}_2=\ddot{x}=u-3\dot{x}-2x=u-3x_2-2x_1\end{array}\right\}\Rightarrow\begin{bmatrix}\dot{x}_1\\ \dot{x}_2\end{bmatrix}=\begin{bmatrix}0 & 1\\ -2 & -3\end{bmatrix}\begin{bmatrix}x_1\\ x_2\end{bmatrix}+\begin{bmatrix}0\\ 1\end{bmatrix}u$$

$$y=4x=4x_1\Leftrightarrow y=\begin{bmatrix}4 & 0\end{bmatrix}\begin{bmatrix}x_1\\ x_2\end{bmatrix},\ A=\begin{bmatrix}0 & 1\\ -2 & -3\end{bmatrix}B=\begin{bmatrix}0\\ 1\end{bmatrix}C=\begin{bmatrix}4 & 0\end{bmatrix}$$ ■

Example 2.3: Find the state space model of the following system:

$$\dddot{x}(t)=3\ddot{x}(t)+2\dot{x}(t)-2x(t)+u_1(t)-6u_2(t)$$

$$y_1=\ddot{x}(t)+u_2(t)$$

$$y_2=\ddot{x}(t)+3x(t)+5u_1(t)$$

$$y_3=-3\ddot{x}(t)+x(t)+5u_2(t)$$

Hence:

$$\left.\begin{array}{l}x=x_1\\ \dot{x}=x_2=\dot{x}_1\\ \ddot{x}=x_3=\dot{x}_2\\ \dddot{x}=3\ddot{x}+2\dot{x}-2x+u_1-6u_2\Leftrightarrow\\ \dot{x}_3=3x_3+2x_2-2x_1+u_1-6u_2\end{array}\right\}\Rightarrow\begin{bmatrix}\dot{x}_1\\ \dot{x}_2\\ \dot{x}_3\end{bmatrix}=\begin{bmatrix}0 & 1 & 0\\ 0 & 0 & 1\\ -2 & 2 & 3\end{bmatrix}\begin{bmatrix}x_1\\ x_2\\ x_3\end{bmatrix}+\begin{bmatrix}0 & 0\\ 0 & 0\\ 1 & -6\end{bmatrix}\begin{bmatrix}u_1\\ u_2\end{bmatrix}\Rightarrow$$

$$\left.\begin{array}{l}y_1=\ddot{x}(t)+u_2(t)\\ y_2=\ddot{x}(t)+3x(t)+5u_1(t)\\ y_3=-3\ddot{x}(t)+x(t)+5u_2(t)\end{array}\right\}\Rightarrow\left.\begin{array}{l}y_1=x_3+u_2\\ y_2=x_3+3x_1+5u_1(t)\\ y_3=-3x_3+x_1+5u_2\end{array}\right\}\Rightarrow$$

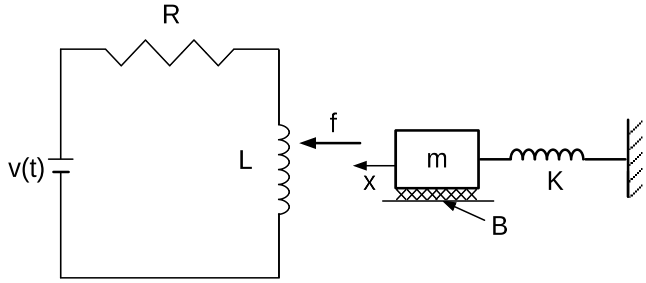
$$\begin{bmatrix}y_1\\ y_2\\ y_3\end{bmatrix}=\begin{bmatrix}0 & 0 & 1\\ 3 & 0 & 1\\ 1 & 0 & -3\end{bmatrix}\begin{bmatrix}x_1\\ x_2\\ x_3\end{bmatrix}+\begin{bmatrix}0 & 1\\ 5 & 0\\ 0 & 5\end{bmatrix}\begin{bmatrix}u_1\\ u_2\end{bmatrix}$$ ■[1]

[1] `A=[0 1 0;0 0 1;-2 2 3]; B=[0 0;0 0;1 -6]; C=[0 0 1;3 0 1;1 0 -3]; D=[0 1;5 0;0 5] sys=ss(A,B,C,D)`

Examples of state space models (NOT ASSESSED MATERIAL)

Example 2.3

Assume the following simple electromechanical that consists of an electromagnet and



The force of the magnetic field is directly related to the current in the *RL* network. The force that is exerted on the object is $f = k_A \frac{i^2}{x^2}$, where k_A is a positive constant. To simplify the analysis we assume that the displacement x is very small and in that small area the current has a linear relationship with the force: $f = k_A i$

Using circuit theory: $\frac{di}{dt} = \frac{1}{L}(v - iR)$

Using Newton's 2nd law: $f - kx - B\dot{x} = m\ddot{x} \Leftrightarrow k_A i - kx - B\dot{x} = m\ddot{x}$

Now, we can define $x_1 = x$, $x_2 = \dot{x}$ and $x_3 = i$. Thus:

$$\dot{x}_3 = \frac{1}{L}(v - x_3 R) \Leftrightarrow \dot{x}_3 = -x_3 \frac{R}{L} + \frac{v}{L}$$

$$\dot{x}_1 = \dot{x} = x_2$$

$$m\dot{x}_2 = k_A x_3 - kx_1 - Bx_2 \Leftrightarrow \dot{x}_2 = -\frac{k}{m} x_1 - \frac{B}{m} x_2 + \frac{k_A}{m} x_3$$

Hence the state space model is:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -k/m & -B/m & -k_A/m \\ 0 & 0 & -R/L \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1/L \end{bmatrix} v \Leftrightarrow \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$$

Now let's assume that we have only one sensor that will return the displacement x:

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

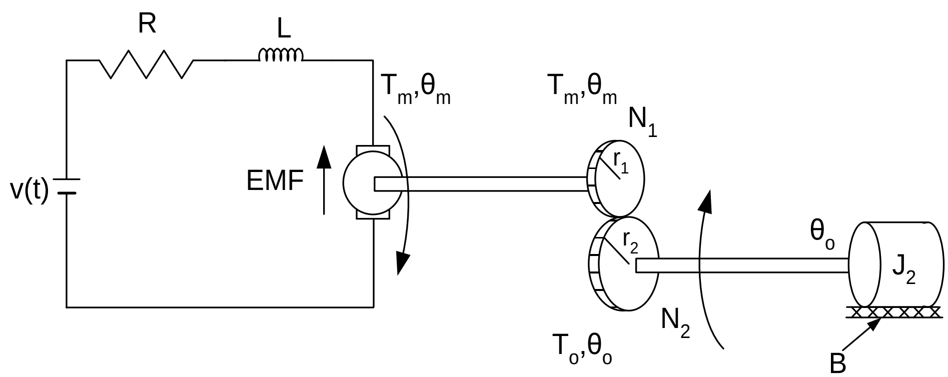
Thus the state space model is:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -k/m & -B/m & -k_A/m \\ 0 & 0 & -R/L \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1/L \end{bmatrix} v$$

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

Example 2.4

Another example is shown in the next figure.



The shaft of the separately excited DC motor is connected to the load J_2 through a gear box.

$$\left.\begin{array}{l} \left.\begin{array}{l} J\ddot{\theta}_0 = T_0 - B\dot{\theta}_0 \\ T_0 = \dfrac{n_2}{n_1} T_m \\ T_m = K_T \varphi i_a \end{array}\right\} \Rightarrow J\ddot{\theta}_0 = \dfrac{n_1}{n_2} K_T \varphi i_a - B\dot{\theta}_0 \\ v_a = i_a R_a + L_a \dfrac{di_a}{dt} + K_T \varphi \dot{\theta}_m \Leftrightarrow v_a = i_a R_a + L_a \dfrac{di_a}{dt} + K_T \varphi \dfrac{n_2}{n_1} \dot{\theta}_0 \end{array}\right\} \Rightarrow$$

$$\left.\begin{aligned} J\ddot{\theta}_0 &= \frac{n_1}{n_2} K_T \phi i_a - B\dot{\theta}_0 \\ v_a &= i_a R_a + L_a \frac{di_a}{dt} + K_T \phi \frac{n_2}{n_1} \dot{\theta}_0 \end{aligned}\right\} \overset{K_2 = K_T \phi \frac{n_1}{n_2}}{\underset{K_1 = K_T \phi \frac{n_2}{n_1}}{\Rightarrow}} \left.\begin{aligned} J\ddot{\theta}_0 &= K_2 i_a - B\dot{\theta}_0 \\ v_a &= i_a R_a + L_a \frac{di_a}{dt} + K_1 \dot{\theta}_0 \end{aligned}\right\}$$

I define $\dot{\theta}_0 = x_1, i_a = x_2$:

$$\left.\begin{aligned} J\dot{x}_1 &= K_2 x_2 - B x_1 \\ v_a &= x_2 R_a + L_a \dot{x}_2 + K_1 x_1 \end{aligned}\right\} \Leftrightarrow \left.\begin{aligned} \dot{x}_1 &= -\frac{B}{J} x_1 + \frac{K_2}{J} x_2 \\ \dot{x}_2 &= -\frac{K_1}{L_a} x_1 - x_2 \frac{R_a}{L_a} + \frac{1}{L_a} v_a \end{aligned}\right\} \Leftrightarrow$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{B}{J} & \frac{K_2}{J} \\ -\frac{K_1}{L_a} & \frac{R_a}{L_a} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L_a} \end{bmatrix} v_a$$

Example 2.4:

It can be proved that a model of the Induction Machine is:

$$\left.\begin{aligned} \frac{d\psi_{sD}}{dt} &= -R_s i_{sD} + u_{sD} \\ \frac{d\psi_{sQ}}{dt} &= -R_s i_{sQ} + u_{sQ} \\ \frac{di_{sD}}{dt} &= \frac{-R_r}{\sigma_1}\psi_{sD} + \frac{-\omega_r L_r}{\sigma_1}\psi_{sQ} + i_{sD}\frac{(L_s R_r + L_r R_s)}{\sigma_1} - i_{sQ}\omega_r - \frac{L_r}{\sigma_1}u_{sD} \\ \frac{di_{sQ}}{dt} &= \frac{-R_r}{\sigma_1}\psi_{sQ} + \frac{\omega_r L_r}{\sigma_1}\psi_{sD} + i_{sQ}\frac{(L_s R_r + L_r R_s)}{\sigma_1} + i_{sD}\omega_r - \frac{L_r}{\sigma_1}u_{sQ} \end{aligned}\right\} \Leftrightarrow$$

$$\begin{bmatrix} \psi_{sD} \\ \psi_{sQ} \\ i_{sD} \\ i_{sQ} \end{bmatrix}^{\bullet} = \begin{bmatrix} 0 & 0 & -R_s & 0 \\ 0 & 0 & 0 & -R_s \\ \frac{-R_r}{\sigma_1} & \frac{-\omega_r L_r}{\sigma_1} & \frac{(L_s R_r + L_r R_s)}{\sigma_1} & -\omega_r \\ \frac{\omega_r L_r}{\sigma_1} & \frac{-R_r}{\sigma_1} & \omega_r & \frac{(L_s R_r + L_r R_s)}{\sigma_1} \end{bmatrix} \begin{bmatrix} \psi_{sD} \\ \psi_{sQ} \\ i_{sD} \\ i_{sQ} \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -\frac{L_r}{\sigma_1} & 0 \\ 0 & -\frac{L_r}{\sigma_1} \end{bmatrix} \begin{bmatrix} u_{sD} \\ u_{sQ} \end{bmatrix}$$

Or:

$$\left.\begin{aligned}
\frac{di_{sD}}{dt} &= -\frac{R_s}{\sigma L_s} i_{sD} + \frac{\omega_r L_m^2}{L_r \sigma L_s} i_{sQ} + \frac{L_m R_r}{L_r \sigma L_s} i_{rd} + \frac{\omega_r L_m}{\sigma L_s} i_{rq} + \frac{1}{\sigma L_s} u_{sD} \\
\frac{di_{sQ}}{dt} &= -\frac{\omega_r L_m^2}{L_r \sigma L_s} i_{sD} - \frac{R_s}{\sigma L_s} i_{sQ} - \frac{\omega_r L_m}{\sigma L_s} i_{rd} + \frac{L_m R_r}{L_r \sigma L_s} i_{rq} + \frac{1}{\sigma L_s} u_{sQ} \\
\frac{di_{rd}}{dt} &= \frac{L_m R_s}{L_r \sigma L_s} i_{sD} - \frac{\omega_r L_m}{\sigma L_r} i_{sQ} - \frac{R_r}{\sigma L_r} i_{rd} - \frac{\omega_r}{\sigma} i_{rq} - \frac{L_m}{L_s \sigma L_r} u_{sD} \\
\frac{di_{rq}}{dt} &= \frac{\omega_r L_m}{\sigma L_r} i_{sD} + \frac{L_m R_s}{L_r \sigma L_s} i_{sQ} + \frac{\omega_r}{\sigma} i_{rd} - \frac{R_r}{\sigma L_r} i_{rq} - \frac{L_m}{L_s \sigma L_r} u_{sQ}
\end{aligned}\right\} \Leftrightarrow$$

$$\begin{bmatrix} \frac{di_{sD}}{dt} \\ \frac{di_{sQ}}{dt} \\ \frac{di_{rd}}{dt} \\ \frac{di_{rq}}{dt} \end{bmatrix} = \begin{bmatrix} -\frac{R_s}{\sigma L_s} & \frac{\omega_r L_m^2}{L_r \sigma L_s} & \frac{L_m R_r}{L_r \sigma L_s} & \frac{\omega_r L_m}{\sigma L_s} \\ -\frac{\omega_r L_m^2}{L_r \sigma L_s} & -\frac{R_s}{\sigma L_s} & -\frac{\omega_r L_m}{\sigma L_s} & \frac{L_m R_r}{L_r \sigma L_s} \\ \frac{L_m R_s}{L_r \sigma L_s} & -\frac{\omega_r L_m}{\sigma L_r} & -\frac{R_r}{\sigma L_r} & -\frac{\omega_r}{\sigma} \\ \frac{\omega_r L_m}{\sigma L_r} & \frac{L_m R_s}{L_r \sigma L_s} & \frac{\omega_r}{\sigma} & -\frac{R_r}{\sigma L_r} \end{bmatrix} \begin{bmatrix} i_{sD} \\ i_{sQ} \\ i_{rd} \\ i_{rq} \end{bmatrix}$$

$$+ \begin{bmatrix} \frac{1}{\sigma L_s} & 0 \\ 0 & \frac{1}{\sigma L_s} \\ -\frac{L_m}{L_s \sigma L_r} & 0 \\ 0 & -\frac{L_m}{L_s \sigma L_r} \end{bmatrix} \begin{bmatrix} u_{sD} \\ u_{sQ} \end{bmatrix}$$

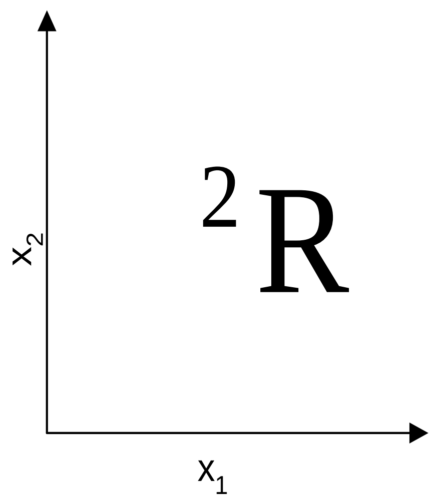
3. State space

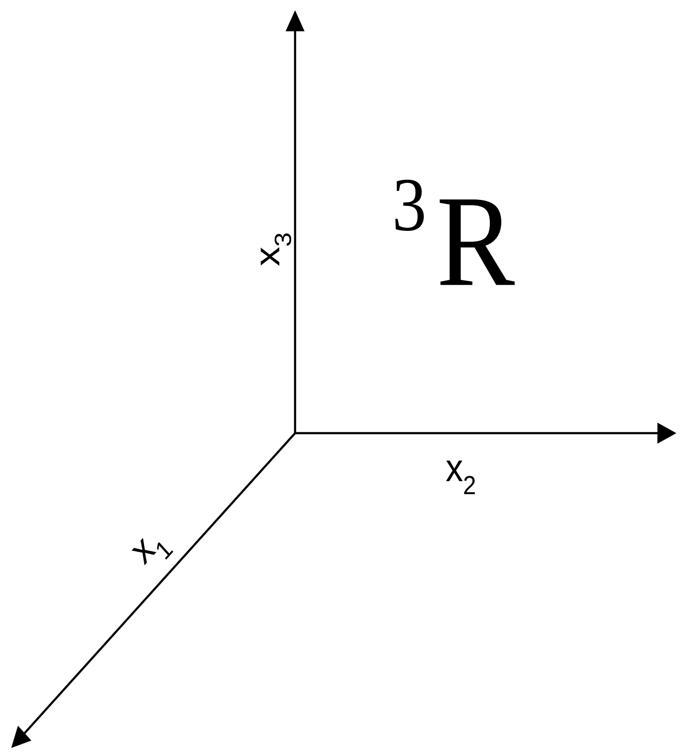
The system's states can be written in a vector form as:

$$\mathbf{x}_1 = [x_1, 0, \cdots, 0]^T,\ \mathbf{x}_2 = [0, x_2, \cdots, 0]^T, \ldots,\ \mathbf{x}_n = [0, 0, \cdots, x_n]^T$$

=> A standard orthogonal basis (since they are linear independent) for an *n*-dimensional vector space called <u>state space.</u>

Examples of state spaces are the state plane (n=2) and state 3D space (n=3),





4. Relation of State Space Models and Transfer Functions

If we have an LTI state space (ss) system, how can we find its TF?

$$\dot{x}(t) = Ax(t) + Bu(t) \overset{LT}{\Rightarrow} sX(s) - x(0) = AX(s) + BU(s) \Rightarrow$$

$$(sI - A)X(s) = BU(s) + x(0) \Rightarrow$$
$$X(s) = (sI - A)^{-1} BU(s) + (sI - A)^{-1} x(0)$$

And from the 2nd equation of the ss system:

$$Y(s) = CX(s) + DU(s) =>$$
$$Y(s) = C\left((sI - A)^{-1} BU(s) + (sI - A)^{-1} x(0)\right) + DU(s)$$

$$Y(s) = \left(C(sI - A)^{-1} B + D\right)U(s) + C(sI - A)^{-1} x(0)$$

By definition TF: $C(sI - A)^{-1} B + D$ and $C(sI - A)^{-1} x(0)$ the response to the IC.

Also: $X(s) = (sI - A)^{-1} BU(s) + (sI - A)^{-1} X(0) \overset{ILT}{\Rightarrow}$

$$x(t) = L^{-1}\left\{(sI - A)^{-1} BU(s)\right\} + L^{-1}\left\{(sI - A)^{-1}\right\} x(0)$$

If u=0 => $X(t) = L^{-1}\left\{(sI - A)^{-1}\right\} X(0)$

So $G(s) = C(sI - A)^{-1}B + D$ is the TF. From linear algebra: $G_{i,j}(s) = \frac{\begin{vmatrix} sI - A & -B_i \\ C_j & D \end{vmatrix}}{|sI - A|}$, where B_i is the i[th] column of the matrix B and C_j is the j[th] row of C.

Hence $|sI - A|$ is the CE of the TF!!!

So: $G(s) = \begin{bmatrix} G_{11}(s) & G_{12}(s) & \dots & G_{1q}(s) \\ G_{21}(s) & G_{22}(s) & \dots & G_{2q}(s) \\ \dots & \dots & \dots & \dots \\ G_{p1}(s) & G_{p2}(s) & \dots & G_{pq}(s) \end{bmatrix}$

$\frac{Y_1}{U_1} = G_{11}, \quad \frac{Y_1}{U_2} = G_{12}, \quad \frac{Y_2}{U_1} G_{21}, \quad \frac{Y_2}{U_2} = G_{22} \dots$

Example 2.5: Find the TF of the following system:

$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -0.5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$ and $y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$

$$\left. \begin{array}{l} |sI - A| = \begin{vmatrix} s & -1 \\ 1 & s + 0.5 \end{vmatrix} = s(s + 0.5) + 1 \\ \begin{vmatrix} s & -1 & 0 \\ 1 & s + 0.5 & -1 \\ 1 & 0 & 0 \end{vmatrix} = 1 \end{array} \right\} \Rightarrow G(s) = \frac{1}{s(s + 0.5) + 1}$$

■

Example 2.6: Find the TF of the following system:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -0.5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u \text{ and } y = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\left.\begin{array}{l} |sI-A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ \begin{vmatrix} s & -1 & 0 \\ 1 & s+0.5 & -1 \\ 1 & 0 & 0 \end{vmatrix} = 1 \end{array}\right\} \Rightarrow G_{1,1}(s) = \frac{1}{s(s+0.5)+1}$$

$$\left.\begin{array}{l} |sI-A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ \begin{vmatrix} s & -1 & 0 \\ 1 & s+0.5 & -1 \\ 0 & 2 & 0 \end{vmatrix} = 1 \end{array}\right\} \Rightarrow G_{2,1}(s) = \frac{2s}{s(s+0.5)+1}$$

Or:

$$G(s) = C(sI-A)^{-1}B + D = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} s & -1 \\ 1 & s+0.5 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix} + 0_{2\times 2}$$

$$\begin{bmatrix} s & -1 \\ 1 & s+0.5 \end{bmatrix}^{-1} = \frac{\begin{bmatrix} s+0.5 & 1 \\ -1 & s \end{bmatrix}}{\begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix}} = \frac{\begin{bmatrix} s+0.5 & 1 \\ -1 & s \end{bmatrix}}{s(s+0.5)+1} \Rightarrow$$

$$G(s) = \frac{1}{s(s+0.5)+1} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} s+0.5 & 1 \\ -1 & s \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \Rightarrow$$

$$G(s) = \frac{1}{s(s+0.5)+1} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} 1 \\ s \end{bmatrix} = \frac{1}{s(s+0.5)+1} \begin{bmatrix} 1 \\ 2s \end{bmatrix}$$

■

Example 2.7: Find the TF of the following system:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -0.5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} u \text{ and } y = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\left.\begin{aligned} &|sI - A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ &\begin{vmatrix} s & -1 & -1 \\ 1 & s+0.5 & 0 \\ 1 & 0 & 0 \end{vmatrix} = s+0.5 \end{aligned}\right\} \Rightarrow G_{1,1}(s) = \frac{s+0.5}{s(s+0.5)+1}$$

$$\left.\begin{aligned} &|sI - A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ &\begin{vmatrix} s & -1 & -1 \\ 1 & s+0.5 & 0 \\ 0 & 2 & 0 \end{vmatrix} = -2 \end{aligned}\right\} \Rightarrow G_{2,1}(s) = \frac{-2}{s(s+0.5)+1}$$

$$\left.\begin{aligned} &|sI - A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ &\begin{vmatrix} s & -1 & -1 \\ 1 & s+0.5 & -1 \\ 1 & 0 & 0 \end{vmatrix} = s+3/2 \end{aligned}\right\} \Rightarrow G_{1,2}(s) = \frac{s+3/2}{s(s+0.5)+1}$$

$$\left.\begin{aligned} &|sI - A| = \begin{vmatrix} s & -1 \\ 1 & s+0.5 \end{vmatrix} = s(s+0.5)+1 \\ &\begin{vmatrix} s & -1 & -1 \\ 1 & s+0.5 & -1 \\ 0 & 2 & 0 \end{vmatrix} = 2s-2 \end{aligned}\right\} \Rightarrow G_{2,2}(s) = \frac{2s-2}{s(s+0.5)+1}$$

Or:

$$G(s)=C(sI-A)^{-1}B+D=\begin{bmatrix}1&0\\0&2\end{bmatrix}\begin{bmatrix}s&-1\\1&s+0.5\end{bmatrix}^{-1}\begin{bmatrix}1&1\\0&1\end{bmatrix}+0_{2\times 2}$$

$$\begin{bmatrix}s&-1\\1&s+0.5\end{bmatrix}^{-1}=\frac{\begin{bmatrix}s+0.5&1\\-1&s\end{bmatrix}}{\begin{vmatrix}s&-1\\1&s+0.5\end{vmatrix}}=\frac{\begin{bmatrix}s+0.5&1\\-1&s\end{bmatrix}}{s(s+0.5)+1}\Rightarrow$$

$$G(s)=\frac{1}{s(s+0.5)+1}\begin{bmatrix}1&0\\0&2\end{bmatrix}\begin{bmatrix}s+0.5&1\\-1&s\end{bmatrix}\begin{bmatrix}1&1\\0&1\end{bmatrix}\Rightarrow$$

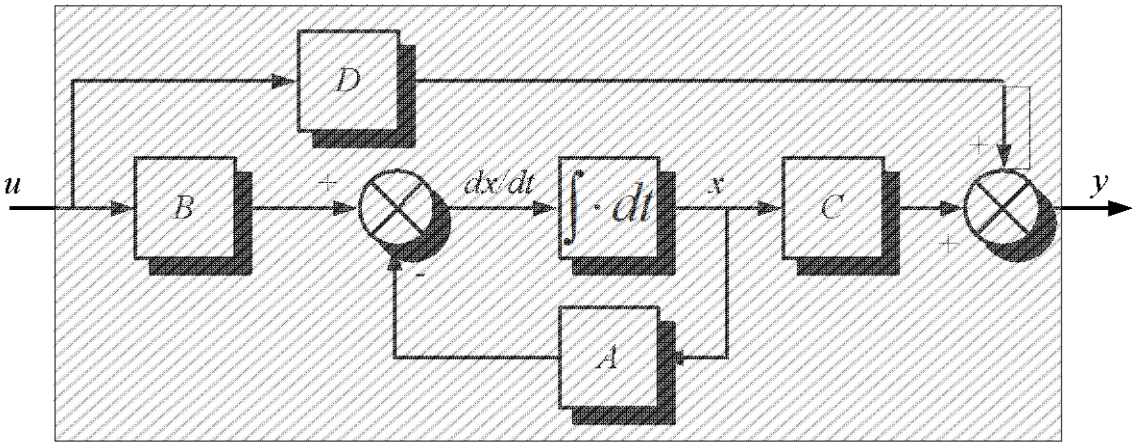
$$G(s)=\frac{1}{s(s+0.5)+1}\begin{bmatrix}s+0.5&1\\-2&2s\end{bmatrix}\begin{bmatrix}1&1\\0&1\end{bmatrix}$$

$$G(s)=\frac{1}{s(s+0.5)+1}\begin{bmatrix}s+0.5&s+0.5+1\\-2&-2+2s\end{bmatrix}$$

■[2]

[2] `A=[0 1;-1 -0.5]; B=[1 1;0 1]; C=[1 0;0 2]; D=zeros(2); [num1,den1]=ss2tf(A,B,C,D,1), [num2,den2]=ss2tf(A,B,C,D,2)`

5. Controllability and Observability



In the above figure we see the block diagram of a generic state space model, deliberately there is a grey box on the top, in order to demonstrate that in reality we cannot see or control the whole system, but we can only control the input signal *u*, and we can see (observe) the output signal *y*. But as it has been previously stated, the most important signal, is the state vector *x*. Hence we want by controlling *u* to be able to influence all the states in *x*, and by observing *y*, we want to be able to get an indication of how *x* behaves. The first concept refers to the "Controllability" of the system and the second on the "Observability" of the system and they are 2 critical properties of a system that must be properly understood.

5.1 Controllability

Example 2.8: Assume the following system: $\dot{x} = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$

By writing it in a form of 2 ODEs: $\begin{cases} \dot{x}_1 = -2x_1 + x_2 + 2u \\ \dot{x}_2 = x_1 - x_2 + u \end{cases}$

It is clear that the signal u influences both ODEs **directly** as it appears in both equations, but also **indirectly** as x_1 and x_2 are coupled. Hence, by changing (how/why/when we will see in chapter 4) the signal u it is possible to influence both states of the system. This system is controllable. ■

Example 2.9: Assume the following system: $\dot{x} = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u$

By writing it in a form of 2 ODEs: $\begin{cases} \dot{x}_1 = -2x_1 + x_2 + 2u \\ \dot{x}_2 = x_1 - x_2 \end{cases}$

It is clear that the signal u influences the ODE of x_1 **directly** as it appears in in the equation, but also x_2 **indirectly** as x_1 appears in the ODE of x_2. Hence, by changing the signal u it is possible to influence both states of the system. This system is controllable. ■

Example 2.10: Assume the following system: $\dot{x} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$

By writing it in a form of 2 ODEs: $\begin{cases} \dot{x}_1 = -2x_1 + 2u \\ \dot{x}_2 = -x_2 + u \end{cases}$

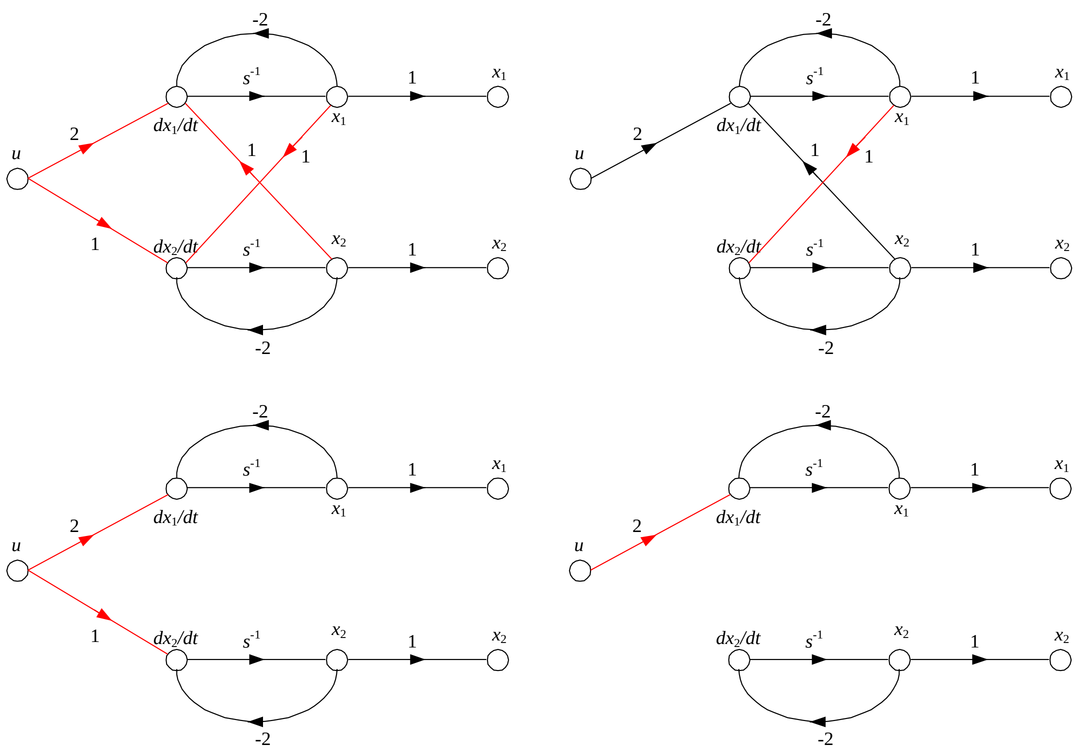
It is clear that the signal u influences both ODEs **directly** as it appears in both equations, but not **indirectly** as x_1 and x_2 are not coupled. Hence, by changing the signal u it is possible to influence both states of the system. This system is controllable. ■

Example 2.11: Assume the following system: $\dot{x} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u$

By writing it in a form of 2 ODEs: $\begin{cases} \dot{x}_1 = -2x_1 + 2u \\ \dot{x}_2 = -x_2 \end{cases}$

It is clear that the signal u cannot influence the second state and hence by changing the signal u it is NOT possible to influence both states of the system. This system is uncontrollable. ■

Example 2.12: The flow chart diagrams of the 4 above systems are shown below and it is clear when x_2 can be influenced:



■

Example 2.13: The transfer functions (assuming C=[3 2]) of the above systems are

$$G(s)=\frac{8s+17}{s^2+3s+1},\ G(s)=\frac{6s+10}{s^2+3s+1},\ G(s)=\frac{8s+10}{s^2+3s+2},$$

$$G(s)=\frac{6s+6}{s^2+3s+2}=\frac{6(s+1)}{(s+1)(s+2)}=\frac{6}{(s+2)}$$

So it is clear that when the system is uncontrollable, there is a pole zero cancelation. ■[3]

It has to be noted here, that the above concept of pole-zero cancelation is more complicated, and it should be used on the matrix $(sI-A)^{-1}B$ *instead. But this is outside the goals of this module.*

Unfortunately, the above methods (ODEs, state flow diagrams, TFs…) break down when the complexity of the system increases. In this case we have a more systematic way to determine the controllability of the system which is to find the rank of the following matrix:

$M_C=\begin{bmatrix} B & AB & A^2B & \cdots & A^{n-1}B \end{bmatrix}$. If the rank of this matrix is less than n then the system is uncontrollable. The rank of a matrix is the number of the linear independent columns/rows. If we have a square matrix, an easy way to determine its rank, is to calculate its determinant and if it is non zero, then the rank is n.

[3] `A=[-2 1;1 -1]; B=[2;1];C=[3 2]; [num,den]=ss2tf(A,B,C,[0])`

Example 2.14: Determine the Controllability of the following system:

$$x = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \Rightarrow AB = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} -3 \\ -1 \end{bmatrix} \Rightarrow$$

$$M_C = \begin{bmatrix} 2 & -3 \\ 1 & -1 \end{bmatrix}$$

And obviously there are 2 LI column/rows. ■[4]

Example 2.15: Determine the Controllability of the following system:

$$x = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \Rightarrow AB = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} -4 \\ -1 \end{bmatrix} \Rightarrow$$

$$M_C = \begin{bmatrix} 2 & -4 \\ 1 & -1 \end{bmatrix}$$

And obviously there are 2 LI column/rows. ■

Example 2.16: Determine the Controllability of the following system:

$$x = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u \Rightarrow AB = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 2 \\ 0 \end{bmatrix} = \begin{bmatrix} -4 \\ 2 \end{bmatrix} \Rightarrow$$

$$M_C = \begin{bmatrix} 2 & -4 \\ 0 & 2 \end{bmatrix}$$

And obviously there are 2 LI column/rows. ■

Example 2.17: Determine the Controllability of the following system:

$$\left.\begin{aligned} \dot{x} &= \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u \\ y &= \begin{bmatrix} 3 & 2 \end{bmatrix} x \end{aligned}\right\} \Rightarrow AB = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} 2 \\ 0 \end{bmatrix} = \begin{bmatrix} -4 \\ 0 \end{bmatrix}$$

$$M_C = \begin{bmatrix} 2 & -4 \\ 0 & 0 \end{bmatrix}$$

And obviously there is only one LI column/row ■[5]

[4] `A=[-2 1;1 -1]; B=[2;1]; rank(ctrb(A,B)), det(ctrb(A,B))`

[5] `A=[-2 0;0 -1]; B=[2;0]; rank(ctrb(A,B)), det(ctrb(A,B))`

5.2 Observability

Example 2.18: Assume the following system:
$$\left.\begin{array}{l}\dot{x}=\begin{bmatrix}-2 & 0\\ 0 & 1\end{bmatrix}x+\begin{bmatrix}2\\0\end{bmatrix}u\\ y=\begin{bmatrix}3 & 1\end{bmatrix}x\end{array}\right\}$$

By writing it in a form of 2 ODEs: $\begin{cases}\dot{x}_1=-2x_1+2u\\ \dot{x}_2=x_2\end{cases}$

Which is clear to see that the 2nd ODE is unstable. BUT as we have mentioned before, we can only observe/measure the output $y=3x_1+x_2$. Hence since x_2 will diverge to +/-∞, we will be able to understand that something "is wrong" by seeing that y also diverges to +/-∞. This system is observable. ■

Example 2.19: Assume the following system:
$$\left.\begin{array}{l}\dot{x}=\begin{bmatrix}-2 & 0\\ 0 & 1\end{bmatrix}x+\begin{bmatrix}2\\0\end{bmatrix}u\\ y=\begin{bmatrix}3 & 0\end{bmatrix}x\end{array}\right\}$$

Now $y=3x_1$ which means that we cannot properly observe the system. This is an unobservable system. ■

Example 2.20: Assume the following system:
$$\left.\begin{array}{l}\dot{x}=\begin{bmatrix}-2 & 1\\ 0 & 1\end{bmatrix}x+\begin{bmatrix}2\\0\end{bmatrix}u\\ y=\begin{bmatrix}3 & 0\end{bmatrix}x\end{array}\right\}$$

By writing it in a form of 2 ODEs: $\begin{cases}\dot{x}_1=-2x_1+x_2+2u\\ \dot{x}_2=x_2\end{cases}$.

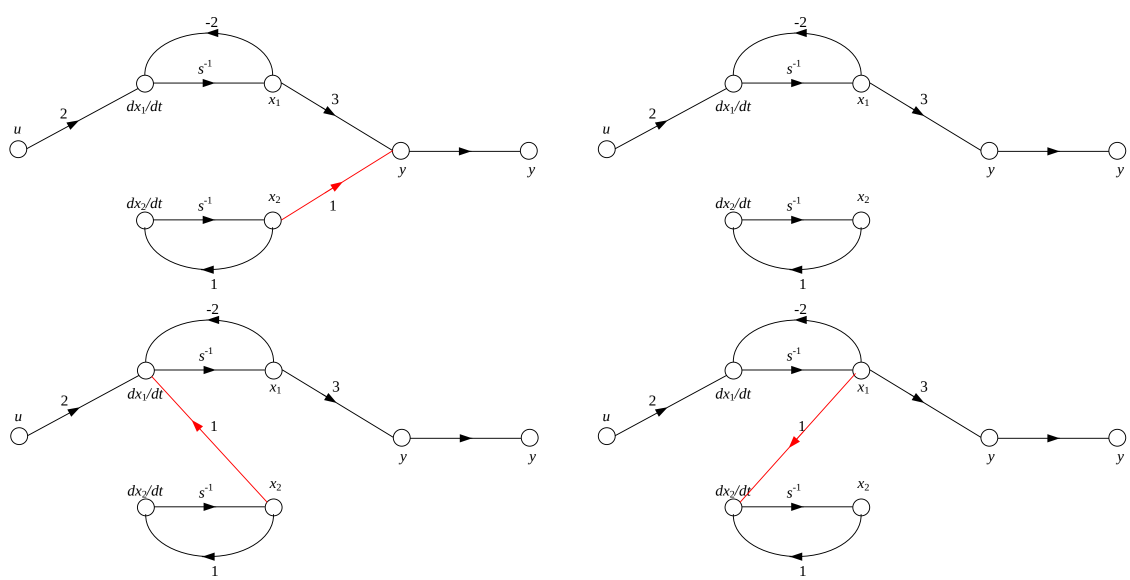
Now, as before, $y=3x_1$ BUT as x_2 influences the ODE of x_1 we will see that "something is wrong" through x_1. The system is observable. ■

Example 2.21: Assume the following system: $\left.\begin{aligned}\dot{x} &= \begin{bmatrix}-2 & 0\\ 1 & 1\end{bmatrix}x + \begin{bmatrix}2\\0\end{bmatrix}u\\ y &= \begin{bmatrix}3 & 0\end{bmatrix}x\end{aligned}\right\}$

By writing it in a form of 2 ODEs: $\begin{cases}\dot{x}_1 = -2x_1 + 2u\\ \dot{x}_2 = x_1 + x_2\end{cases}$.

Now, as before, $y = 3x_1$ BUT now even though x_1 influences the ODE of x_2, the ODE of x_1 is still decoupled from x_2 and hence by observing y we will not be able to observe that x_2 is unstable. This system is unobservable. ■

Example 2.22: The flow chart diagrams of the 4 above systems are shown below and it is clear when x_2 can be observed:



A more efficient way to test the observability is to determine the rank of the following matrix: $M_O = \begin{bmatrix}C & CA & CA^2 & \cdots & CA^{n-1}\end{bmatrix}^T$. If the rank of this matrix is less than n then the system is unobservable.

Example 2.23: Determine the Observability of the following system:

$$\left.\begin{aligned}\dot{x} &= \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \\ y &= \begin{bmatrix} 3 & 0 \end{bmatrix} x \end{aligned}\right\} \Rightarrow CA = \begin{bmatrix} 3 & 0 \end{bmatrix} \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} = \begin{bmatrix} -6 & 0 \end{bmatrix}$$

$$M_O = \begin{bmatrix} 3 & 0 \\ -6 & 0 \end{bmatrix}$$

And obviously there is only one LI column/row ■

Example 2.24: Determine the Observability of the following system:

$$\left.\begin{aligned}\dot{x} &= \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \\ y &= \begin{bmatrix} 3 & 2 \end{bmatrix} x \end{aligned}\right\} \Rightarrow CA = \begin{bmatrix} 3 & 2 \end{bmatrix} \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} = \begin{bmatrix} -6 & -2 \end{bmatrix}$$

$$M_O = \begin{bmatrix} 3 & 2 \\ -6 & -2 \end{bmatrix}$$

And obviously there are 2 LI column/rows ■[6]

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[6] `A=[-2 0;0 -1]; B=[2; 1]; C=[3 2]; rank(obsv(A,C))`

Tutorial Exercise II

1. Derive a state space representation of the mass spring system assuming that the system has 2 outputs: the displacement and the velocity.
2. Repeat Question 1 assuming that the displacement is the only system output.
3. Find the state space model of the following system:

$$\ddot{x} + 6\dot{x} + 5x = u(t)$$
$$y = 4\dot{x} + x$$

4. A state space model is given by

$$A = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 \\ 6 & 7 & 8 & 9 & 10 \\ 11 & 12 & 13 & 14 & 15 \\ 16 & 17 & 18 & 19 & 20 \\ 21 & 22 & 23 & 24 & 25 \end{bmatrix},\ B = \begin{bmatrix} -0.1 & -0.2 & -0.3 \\ -0.4 & -0.5 & -0.6 \\ -0.7 & -0.9 & -1 \\ -1.1 & -1.2 & -1.3 \\ -1.4 & -1.5 & -1.6 \end{bmatrix},$$

$$C = \begin{bmatrix} 1 & 1 & 2 & 2 & 3 \\ 0 & 0 & 0 & -1 & 152 \end{bmatrix},\ D = 0$$

(a) What is the order of the system?
(b) How many inputs/ outputs do we have in this system?
(c) What are the dimensions of the matrix *D*?

5. Find the state space model of:

(a)
$$\left.\begin{aligned} & x^{(4)} = 3x^{(3)} + 4x'' - 3x' + x + u_1 - 3u_2 + 5u_3 \\ & y_1 = x^{(3)} + u_1 \\ & y_2 = x^{(4)} + 1.2x' + u_3 - u_1 \\ & y_3 = x \end{aligned}\right\}$$

(b)
$$\left.\begin{aligned}\dot{x}_1 &= 3x_1 + 3x_2 + u_1 + u_2 + u_3 + u_4 \\ \dot{x}_2 &= 3x_2 + u_1 - 2u_3 \\ y_1 &= x_1 \\ y_2 &= x_1 + 3x_2 + u_1 + u_2 \\ y_3 &= x_1 - 2x_2 + u_3 + u_4\end{aligned}\right\}$$

In each case find:

- The order of the system?
- How many inputs/ outputs do we have in this system?

6. Find the transfer function of a system with:

$$A = \begin{bmatrix} 1 & 2 \\ 3 & 4 \end{bmatrix}, B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, C = \begin{bmatrix} 1 & 1 \end{bmatrix}, D = 0.$$

7. Find the transfer function of a system with:

$$A = \begin{bmatrix} 1 & 2 \\ 3 & 4 \end{bmatrix}, B = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}, C = \begin{bmatrix} 1 & 1 \end{bmatrix}, D = \begin{bmatrix} 0 & 0 \end{bmatrix}.$$

8. Find the transfer function of a system with:

$$A = \begin{bmatrix} 1 & 2 \\ 3 & 4 \end{bmatrix}, B = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}, C = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}, D = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}.$$

9. What is the characteristic equation in Q.6-8? What is the system order? Is that system stable? Why? Are these systems observable/controllable?