

ZDM

(Another Taylor Series' Heaven!)

The system is described by:

$$\dot{\mathbf{x}} = F(\mathbf{x}), \quad \text{when } H(\mathbf{x}) > 0$$

$$\mathbf{x} \rightarrow R(\mathbf{x}), \quad \text{when } H(\mathbf{x}) = 0$$

$$\Sigma = \{x : H(\mathbf{x}) = 0\}$$

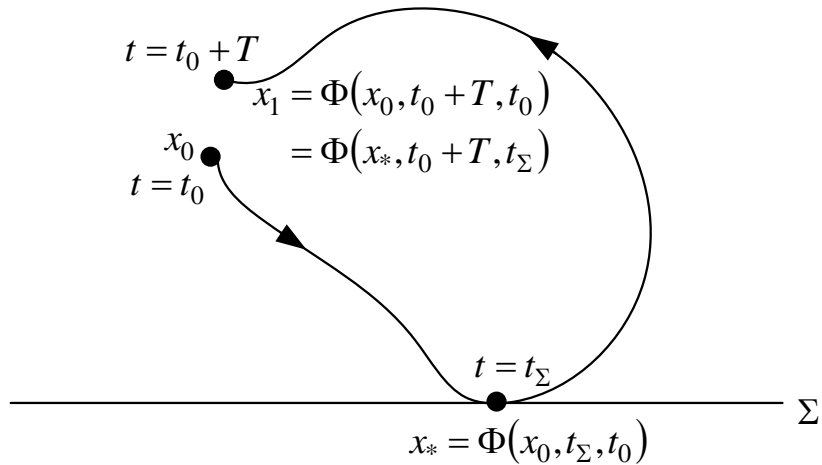
$$v(\mathbf{x}) = \frac{dH(\mathbf{x})}{dt} = \frac{dH(\mathbf{x})}{d\mathbf{x}} \frac{d\mathbf{x}}{dt} = H_x(\mathbf{x})F(\mathbf{x})$$

$$a(\mathbf{x}) = \frac{d^2H(\mathbf{x})}{dt^2} = (H_x(\mathbf{x})F(\mathbf{x}))_x F(\mathbf{x})$$

At the grazing point:

$$H(\mathbf{x}_*) = 0, v(\mathbf{x}_*) = 0, a(\mathbf{x}_*) = a_* > 0$$

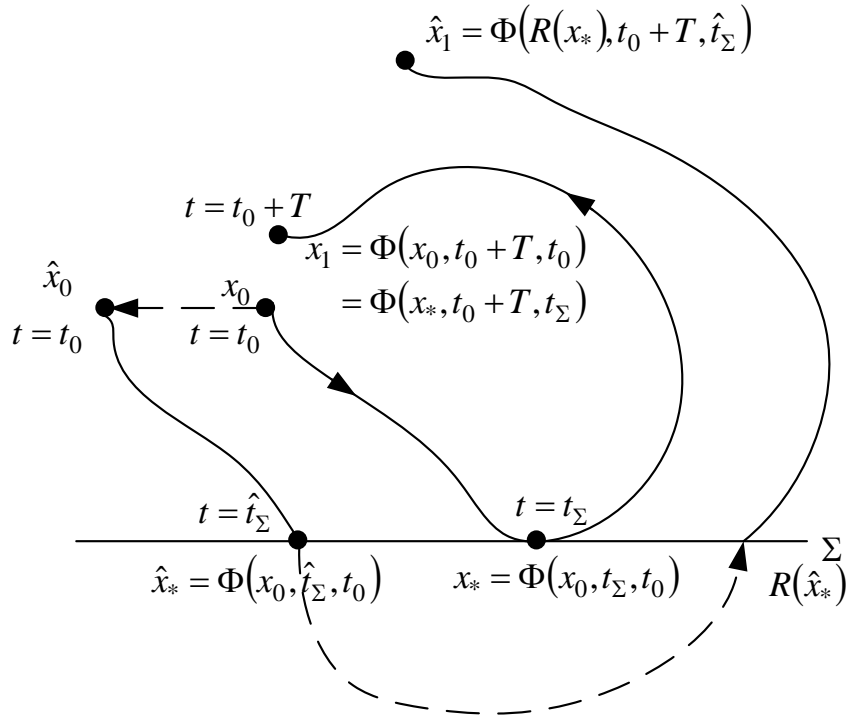
Let's assume an orbit that (near) grazes a switching manifold:



We can define the Poincare map as:

$$x_1 = P(x_0) = \Phi(x_*, T + t_0, t_\Sigma) \Phi(x_0, t_\Sigma, t_0) \quad (1)$$

To study the stability of this orbit we follow the classical Lyapunov method. This means that we add a perturbation and we see how the perturbations behave:



Then if we use the same map as in (1) there is obviously an error as the new orbit is different than the original one.

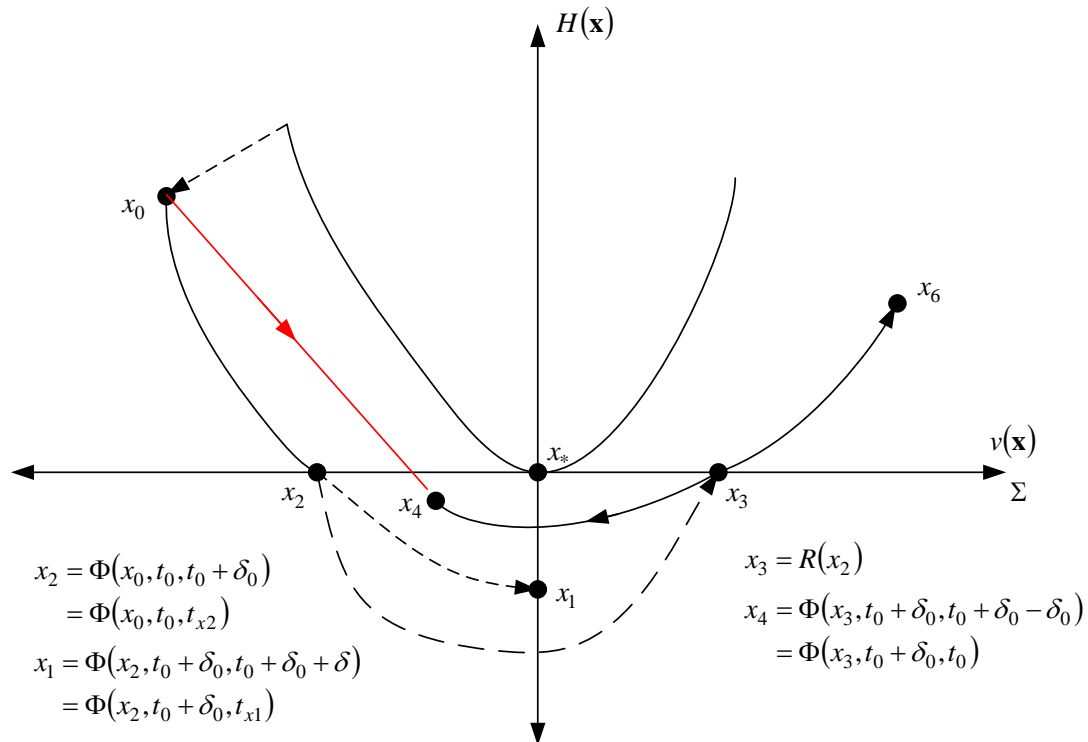
Thus we need a map that will overcome this problem. This map, that will be applied at a neighbourhood around the grazing point, and will take into account the possibility of crossing the switching manifold. So I expect something like this:

$$x \mapsto \begin{cases} x, & \text{if the orbit that starts in } x \text{ does not cross } \Sigma \text{ or grazes } \Sigma \\ ZDM(x) & \text{if the orbit that starts in } x \text{ crosses } \Sigma \text{ or grazes } \Sigma \end{cases} \quad (2)$$

So lets zoom in an orbit that just grazes Σ (all the previous symbols are re-initialised).

Before we do that let's assume that the switching manifold is $h(\mathbf{x}) = x_1$, in that case

$v(\mathbf{x}) = x_2$:



The time needed to go from x_0 to x_6 is the same as x_4 to x_6 , i.e. by ignoring the impact.

From the above diagram we have that:

$$V(x_1) = 0, \quad H(x_2) = 0, \quad H(x_3) = 0 \tag{3}$$

I define as:

$$H_{\min}(x_0) = \min\{\Phi(x_0, t, t_0)\} = \min\{\Phi(x_0, t_0 + \delta, t_0)\} = H(x_1) \equiv -y^2 \tag{6}$$

For a generic point x near x_* (like x_1, x_2, x_3 and x_4) we have:

$$F(x) = F(x_*) + F_x(x_*)\Delta x + HOT \quad (7)$$

As $F(x_*)$ is not zero we can say that this term dominates the RHS of (7) and thus all other terms can be neglected:

$$F(x) = F(x_*) \quad (8)$$

So from now on we will use $F(x_*)$ instead of $F(x_1), F(x_2), F(x_3),$ & $F(x_4)$.

Similarly for $a(x_*) = a_*$ instead of $a(x_1), a(x_2), a(x_3),$ & $a(x_4)$

A point near x_1 is given by: $\Phi(x_1, t_{x1}, t_{x1} + t)$. Using a TS wrt time around $t=0$:

$$\Phi(x_1, t_{x1}, t_{x1} + t) = \Phi(x_1, t_{x1}, t_{x1}) + \left. \frac{\partial \Phi(x_1, t_{x1}, t_{x1} + t)}{\partial t} \right|_{t=0} t + \left. \frac{\partial^2 \Phi(x_1, t_{x1}, t_{x1} + t)}{\partial^2 t} \right|_{t=0} \frac{t^2}{2} + HOT$$

Now this flow can be evaluated for $t = -\delta$ to get to x_2 and for $t = -\delta_1$ to get to x_0 .

This will allow us to connect x_0 with x_1 using a simple expression:

$$\Phi(x_1, t_{x1}, t_{x1} + t) \approx x_1 + F(x_1)t \quad (8b)$$

$$\text{and by setting } t = -\delta: \text{ I have } x_2 \approx x_1 - F(x_1)\delta \quad (9)$$

$$\text{And using (8) } x_2 \approx x_1 - F(x_*)\delta \quad (10)$$

$$\text{Similarly: } x_0 \approx x_1 - F(x_*)\delta_1 \quad (11)$$

$$\text{Similarly: } x_0 \approx x_2 - F(x_*)\delta_0 \quad (12)$$

Now using the jump map I can relate x_2 with x_3 :

$$x_3 = R(x_2) = x_2 + W(x_2)v(x_2) \quad (13)$$

Hence Using (12):

$$x_3 = R(x_2) = x_0 + F(x_*)\delta_0 + W(x_0 + F(x_*)\delta_0)v(x_0 + F(x_*)\delta_0) \quad (14)$$

A point near x_3 is given by: $\Phi(x_3, t_{x_2}, t_{x_2} + t)$.

Using a TS wrt time around $t=0$:

$$\begin{aligned} \Phi(x_3, t_{x_2}, t_{x_2} + t) &= \Phi(x_3, t_{x_2}, t_{x_2}) + \left. \frac{\partial \Phi(x_3, t_{x_2}, t_{x_2} + t)}{\partial t} \right|_{t=0} t + HOT \Leftrightarrow \\ \Phi(x_3, t_{x_2}, t_{x_2} + t) &= x_3 + F(x_3)t + HOT \end{aligned}$$

$$\text{Evaluating this at } t = -\delta_0: x_4 = x_3 - F(x_3)\delta_0 + HOT \quad (15)$$

$$\text{And by neglecting HOT and using (8): } x_4 = x_3 - F(x_*)\delta_0 \quad (16)$$

Hence combining (16) and (14):

$$x_4 = x_0 + W(x_0 + F(x_*)\delta_0)v(x_0 + F(x_*)\delta_0) \quad (17a)$$

$$\text{Or } x_4 = x_0 + W(x_2)v(x_2) \quad (17b)$$

In (17b) we have 2 unknown factors: $W(x_2)$ and $v(x_2)$. As the point x_2 is near x_* we can replace $W(x_0 + F(x_*)\delta_0)$ with $W(x_*)$. Thus I simply need to find $v(x_2)$.

Using (10): $x_2 = x_1 - F(x_*)\delta$

$$\text{Thus } v(x_2) = v(x_1 - F(x_*)\delta) \quad (18)$$

Using a TS on (18) wrt x at x_1 :

$$v(x_1 - F(x_*)\delta) = v(x_1) - v_x(x_1)F(x_*)\delta + HOT$$

Originally we have seen that $v(x_1) = 0$, hence:

$$\begin{aligned} v(x_2) &\approx -v_x(x_1)F(x_*)\delta \Leftrightarrow \\ v(x_2) &= \underbrace{-v_x(x_*)F(x_*)}_{a(x_*)}\delta \Leftrightarrow v(x_2) = -a_* \delta \end{aligned} \quad (19)$$

Thus my only unknown now is δ . To find that I will use (8b) and I will evaluate

the function H on that general point: $H\left(x_1 + F(x_1)t + F_x(x_1)F(x_1)\frac{t^2}{2}\right)$

Now, by taking the TS wrt x around x_1

$$\begin{aligned}
H\left(x_1 + F(x_1)t + F_x(x_1)F(x_1)\frac{t^2}{2}\right) &= H(x_1) + H_x(x_1)\left(F(x_1)t + F_x(x_1)F(x_1)\frac{t^2}{2}\right) + \\
&\quad + H_{xx}(x_1)\frac{\left(F(x_1)t + F_x(x_1)F(x_1)\frac{t^2}{2}\right)^2}{2} + HOT \\
&= H_{\min}(x_0) + \underbrace{H_x(x_1)F(x_1)}_{v(x_1)=0}t + H_x(x_1)F_x(x_1)F(x_1)\frac{t^2}{2} \\
&\quad + H_{xx}(x_1)F(x_1)F(x_1)\frac{t^2}{2} + HOT \\
&\approx -y^2 + (H_x(x_1)F_x(x_1)F(x_1) + H_{xx}(x_1)F(x_1)F(x_1)) \\
&= -y^2 + a(x_1)\frac{t^2}{2} \Leftrightarrow \\
H(\Phi(x_1, t_{x1}, t_{x1} + t)) &= -y^2 + a_*\frac{t^2}{2} \tag{20}
\end{aligned}$$

By evaluating (20) at $t = -\delta$ I have that

$$H(\Phi(x_1, t_{x1}, t_{x1} - \delta)) = 0 = -y^2 + a_*\frac{\delta^2}{2} \Rightarrow \delta = \sqrt{\frac{2}{a_*}}y \tag{21}$$

Thus using (17b), (19) and (21):

$$x_4 = x_0 - W(x_*)a_*\sqrt{\frac{2}{a_*}}y \Leftrightarrow$$

$$x_4 = x_0 - W(x_*)\sqrt{2a_*}y \tag{22}$$

Thus we have the ZDM map:

$$ZDM(x) = x - W(x_*)\sqrt{2a_*}y$$

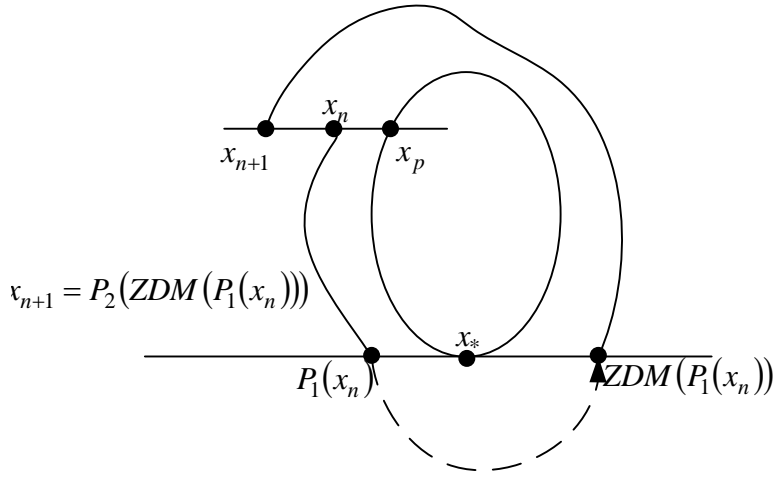
It is interesting to point that the Jacobian of that map is singular at the point of grazing as:

$$\frac{\partial ZDM(x)}{\partial x} = I - W(x_*)\sqrt{2a_*} \frac{\partial y}{\partial x} \quad (23)$$

$$\text{But } \frac{\partial y}{\partial x} = \frac{\partial \sqrt{-H_{\min}(x)}}{\partial x} \approx \frac{\partial \sqrt{-H(x_1)}}{\partial x} = -\frac{\partial H(x_1)}{\partial x} \frac{1}{2\sqrt{-H(x_1)}} \quad (24)$$

And as $x \rightarrow x_*$ I have $H(x_1) \rightarrow 0$ and thus: $\frac{\partial y}{\partial x} \rightarrow \pm\infty$

Now let's see how we can use this map.



The overall map is $x_{n+1} = P_2(ZDM(P_1(x_n)))$, in the case where $x_n = x_p$ I have:

$$x_{n+1} = P_2 \left(\underbrace{\underbrace{ZDM \left(\underbrace{P_1(x_p)}_{x^*} \right)}_{x^*}} \right) = x_p, \text{ i.e. indeed } x = x_p \text{ is a fixed point of our map.}$$

Going back to the definition of the map:

$$x_{n+1} = P_2(ZDM(P_1(x_n))) \quad (25)$$

In order to simplify the analysis I will semi-linearise that expression. We will still not get an analytic form which we can use to find eigenvalues but it will give us an easier form.

$$P_1(x_n) = P_1(x_p) + \frac{\partial P_1(x_n)}{\partial x_n} (x_n - x_p) = x_* + N_1(x_n - x_p) \quad (26)$$

Now let's apply the ZDM on that point:

$$ZDM(x_* + N_1(x_n - x_p)) = x_* + N_1(x_n - x_p) - W(x_*) \sqrt{2a_*} \sqrt{-H_{\min}(x_* + N_1(x_n - x_p))}$$

Now the map P_2 :

$$P_2(x_* + N_1(x_n - x_p) - W(x_*)\sqrt{2a_*}\sqrt{-H_{\min}(x_* + N_1(x_n - x_p))}) \quad (27)$$

And using a TS wrt x around x_* :

$$\begin{aligned} & P_2(x_*) + \left. \frac{\partial P_2(x)}{\partial x} \right|_{x=x_*} \left(N_1(x_n - x_p) - W(x_*)\sqrt{2a_*}\sqrt{-H_{\min}(x_* + N_1(x_n - x_p))} \right) \\ &= P_2(x_*) + N_2 \left(N_1(x_n - x_p) - W(x_*)\sqrt{2a_*}\sqrt{-H_{\min}(x_* + N_1(x_n - x_p))} \right) \\ &= x_p + N_2 N_1(x_n - x_p) - N_2 W(x_*)\sqrt{2a_*}\sqrt{-H_{\min}(x_* + N_1(x_n - x_p))} \end{aligned}$$

We can simplify this expression even more by using a TS on $H_{\min}(x_* + N_1(x_n - x_p))$:

$$\begin{aligned} H_{\min}(x_* + N_1(x_n - x_p)) &= \underbrace{H_{\min}(x_*)}_0 + \left. \frac{\partial H_{\min}(x)}{\partial x} \right|_{x=x_*} N_1(x_n - x_p) \\ &= H_{x_{\min}}(x_*) N_1(x_n - x_p) \\ &= H_x(x_*) N_1(x_n - x_p) \end{aligned}$$

The TS expansion of (25) wrt x_n around x_p will give:

$$\begin{aligned} x_{n+1} &= P_2(ZDM(P_1(x_p))) + \left. \frac{\partial P_2(ZDM(P_1(x_n)))}{\partial x_n} \right|_{x_n=x_p} (x_n - x_p) \Leftrightarrow \\ x_{n+1} &= x_p + \left. \frac{\partial P_2(ZDM(P_1(x_n)))}{\partial x_n} \right|_{x_n=x_p} (x_n - x_p) \end{aligned} \quad (26)$$

The Jacobian of this map:

$$\left. \frac{\partial P_2(ZDM(P_1(x_n)))}{\partial x_n} \right|_{x_n=x_p} = \left. \frac{\partial P_2(ZDM(P_1(x_n)))}{\partial ZDM(P_1(x_n))} \right|_{x_n=x_p} \left. \frac{\partial ZDM(P_1(x_n))}{\partial P_1(x_n)} \right|_{x_n=x_p} \left. \frac{P_1(x_n)}{\partial x_n} \right|_{x_n=x_p}$$

Now $\left. \frac{P_1(x_n)}{\partial x_n} \right|_{x_n=x_p} = N_1$ and if $x_n = x_p$ I have that $P_1(x_n) = x_*$ and thus

$$ZDM(x_*) = x_*. \text{ Hence } \left. \frac{\partial P_2(ZDM(P_1(x_n)))}{\partial ZDM(P_1(x_n))} \right|_{x_n=x_p} = \left. \frac{\partial P_2(\hat{x})}{\partial \hat{x}} \right|_{\hat{x}=x_*} = N_2$$

Similarly, $\frac{\partial ZDM(P_1(x_n))}{\partial P_1(x_n)} \Big|_{x_n=x_p} = \frac{\partial ZDM(\hat{x})}{\partial P_1(\hat{x})} \Big|_{\hat{x}=x_p} = N_1$

Thus: $\frac{\partial P_2(ZDM(P_1(x_n)))}{\partial x_n} = N_2 J_{ZDM} N_1$ (27)